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Revisions are shown in red.

Question 61, p. 44

The W10×22 steel beam ($F_y = 50$ ksi) shown in the figure is braced at unknown intervals.

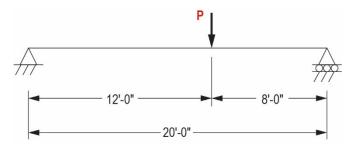
Work either the ASD or the LRFD version of the question. Assume $c_b = 1.0$.

<u>ASD</u>

The allowable flexural strength (ft-kips) of the beam is most nearly:

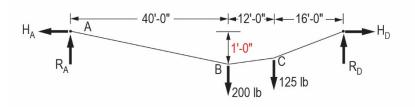
<u>LRFD</u>

The design moment capacity ϕM_n (ft-kips) of the beam is most nearly:



Question 73, p. 56 Option B should read as follows: O B. ASD = 21.3 LRFD = 32.1

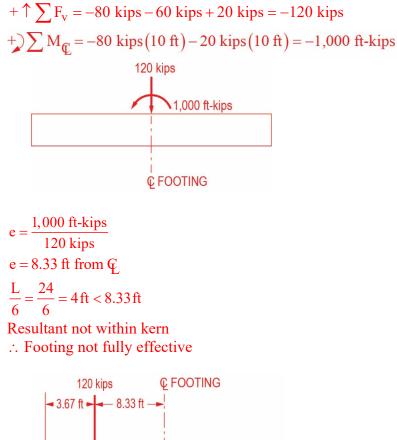
Solution 54, p. 84

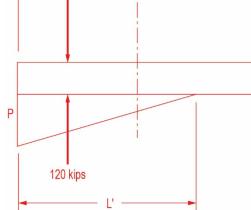


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Solution 70, p. 92

Weight of footing = 2.5 kips/ft(24 ft) = 60 kips





Resultant of soil pressure must align with eccentric resultant load. L' is the effective length of the triangular soil pressure pattern.

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Solution 70, p. 92 (Continued)

$$\therefore 3.67 \text{ ft} = \frac{L'}{3} \rightarrow L' = 3(3.67 \text{ ft}) = 11.01 \text{ ft}$$
$$\frac{1}{2} \text{PL'} = \frac{1}{2} \text{P}(11.01 \text{ ft}) = 120 \text{ kips} \rightarrow \text{P} = \frac{2(120 \text{ kips})}{11.01 \text{ ft}} = 21.8 \text{ kips/ft}$$
$$\text{P}_{\text{max}} = \frac{\text{P}}{8 \text{ ft}} = \frac{21.8 \text{ kips/ft}}{8 \text{ ft}} = 2.72 \text{ kips/ft}^2$$

THE CORRECT ANSWER IS: C

Solution 73, p. 93 AISC, 14th ed.

ASD:

 $F_{nv} = 27 \text{ ksi}$ $F_{nv}/\Omega = 13.5 \text{ ksi}$ Allowable load = 2(13.5)(0.79) = 21.33 kips LRFD: $\phi R_n = \phi F_{nv} A_b$ $\phi F_{nv} = 20.3 \text{ ksi} (A307 \text{ bolts})$ $\phi R_n = (20.3)(0.79)(2) = 32.07 \text{ kips}$ Table J3.2

Alternate solution, use Table7-1