Revisions are shown in red.

Question 801, p. 180

Requirement (b) should read as follows:

(b) Determine the design wind pressure and seismic design force on the parapet. For wind, use the provisions of ASCE 7 Ch. 30 Part 6 and neglect corner zones. (Consider interior zones only.)

Solution 803, p. 230

The last five lines of Requirement (c) should read as follows:

Alternatively, the provisions of Sec. 25.4.2.3 may be used

$$\ell_{d} = \frac{3}{40} \frac{f_{y} \Psi_{t} \Psi_{e} \Psi_{s}}{\lambda f_{c}' \left(\frac{c_{b} + K_{tr}}{d_{b}}\right)} d_{b}$$
ACI Eq. 25.4.2.3a
where $\frac{c_{b} + K_{tr}}{d} = \frac{3.313 + 0}{0.625} = 5.3 \le 2.5$ Use 2.5
 $\ell_{d} = \frac{3}{40} \frac{60(1.0)(1.0)(0.8)}{1.0(5)(2.5)} 0.625 = 12.7$ in.
Class B splice = (1.3)(12.7) = 16.5 NG

Solution 804, p. 232

Requirement (b) should read as follows:

(b) Nailing requirements of shear wall:NDS SDPWS Table 4.3A
$$15/32"$$
 wood structural panels-sheathingw/ 8d nails @ 6" o.c. @ panel edgesand @ 12" o.c. @ intermediate supports, $V_w = 730$ plfFootnote 3 specific adjustment factor: $= [1 - (0.5 - G)]$ Hem-Fir G = 0.43Hem-Fir G = 0.43NDS Table 12.3.3A $= [1 - (0.5 - 0.43)] = 0.93$ NDS Table 12.3.3A $V_{Allow} = \frac{730 \text{ plf}}{2.0} \times 0.93 = 340 \text{ plf} > 270 \text{ plf}$ OKBottom plate to blocking between trussesNDS Table 12NFor 16d nails and 2×4 bottom plate ($t_s = 1 1/2"$)NDS Table 12N $Z = 122$ lbPenetration into main member (blocking):

6 D = 6 (0.162) = 0.972"

p = 31/2 - 11/2 - 3/4 = 11/4"

10 D = 10(0.162) = 1.62"

 \therefore 6 D \rightarrow use adj. factor footnote 3

$$z' = 122 lb \times C_D \times p/10 d$$

 $= 122 \times 1.6 \times 1.25 / 1.62 = 150$ lb / nail

Required spacing
$$=\frac{150}{270}=0.56'=6.7"$$

: Attach bottom plate to blocking with 16d nails @ 6" o.c. (max.)

Add second-floor diaphragm loads

$$V_{DIA} = \frac{3,130 \text{ lb}}{7 \times 30 \text{ ft}} = 14.9 \text{ plf}$$

V = 270 plf + 15 plf
V = 285 plf

804. (Continued)

Blocking between trusses to top plate (wall below) Use 16d toe nails z = 122 lb (from above) Penetration of toe nail into main member (top plate): $p = \ell \cos 30^\circ - \ell/3 = 31/2 (\cos 30^\circ) - \frac{31/2}{3} = 1.86"$

 $\therefore p > 10 d$

 $z' = 122 lb \times C_D \times C_{tn}$

 $= 122 \times 1.6 \times 0.83 = 162$ lb / nail

Required spacing $=\frac{162}{285 \text{ plf}} = 0.57 \text{ ft} = 6.82 \text{ in}.$

 \therefore Attach blocking to top plate with 16d toe nails @ 6 in. o.c. max. Alternately, provide metal framing clips from blocking to top plate with correct combination of capacity and spacing for overall resistance of 285 plf

Net uplift holdown forces:

At location adjacent to balcony: $M_{gross} = 56,425$ ft-lb (from Requirement (a))

 $M_{0.6D} = 0.6(20 \text{ psf})(20 \text{ ft})(10 \text{ ft})(10 \text{ ft}/2)$

+ 0.6(15 psf)(20 ft)(10 ft)(10 ft/2) = 21,000 ft-lb

 $M_{net} = 56,425 - 21,000 = 35,425$ ft-lb

Distance between holdown bolts ≈ 10 ft -0.75 ft = 9.25 ft

$$T_{@holdown} = \frac{M}{b} = \frac{35,425 \text{ ft-lb}}{9.25 \text{ ft}} = 3,830 \text{ lb}$$

$$\begin{split} T_{@\ holdown} &= T_{shear\ wall} + T_{header} \\ At \ location \ adjacent \ to \ 10\mbox{-ft opening:} \\ T_{header} &= 440 \ plf \ (10 \ ft/2) - 0.6(20 \ psf \ + 15 \ psf)(20 \ ft) \ (10 \ ft/2) = 100 \ lb \end{split}$$

 \therefore T_{@ holdown} = 3,830 + 100 = 3,930 lb

NDS Table 12N

Solution 804, p. 235

Requirement (d) should read as follows:



Note: This detail outlines one of numerous possible configurations. The key components for the load path include:

- 1. Plywood wall sheathing
- 2. Boundary nailing
- 3. Bottom plate
- 4. Nailing of plate to plywood floor sheathing and blocking
- 5. Nailing of blocking to double top plate
- 6. Boundary nailing
- 7. Plywood wall sheathing